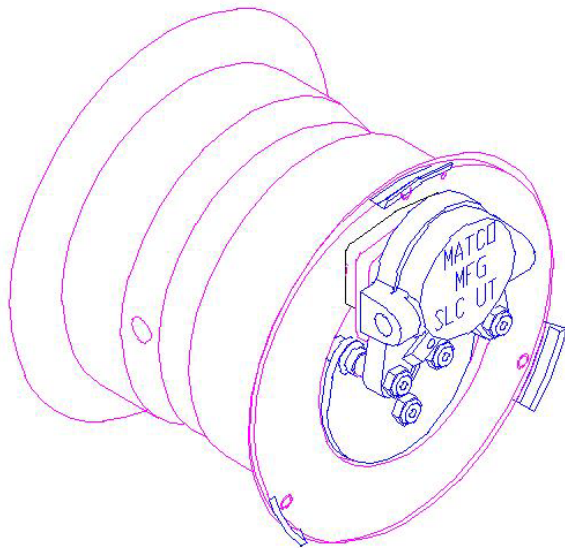


MATCO mfg

Wheels & Brakes

MH SERIES Wheels and Brakes



Technical Service Guide

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A. MH SERIES SIX-INCH WHEEL & BRAKE ASSEMBLY

DIMENSIONS

The MH6 series wheel is a six-inch wheel with a 5.375-inch width and an additional 1.24-inch caliper spacing. Bearing spacing is 2.00 inches and axle spacing is 2.00 inches. The total weight of this wheel and brake assembly is 4.4 pounds. The bearing axle diameter is .625 inches for the MH6B, MH6B.62D, and the MH6BD.62. and .750 inches for the MH6B.75, MH6B.75D, MH6BD.75, and MH6BDXT.75.

FEATURES

The MH Series Wheel is now produced as a CNC spun wheel with a Tenzalloy hub. The CNC spun wheel ensures the highest accuracy and repeatability without the problems associated with stamped wheels from aluminum. These wheels have a specially designed shoulder to ensure a better seal and support of the tire bead seat, and the material thickness is 30% greater than the older stamped wheel. The MH series wheel uses precision sealed ball bearings that have been designed and rigorously tested to resist bearing fatigue. This wheel features a four-inch brake assembly available in three configurations for excellent braking performance to match the needs of the aircraft.

The single caliper MH6B can easily be upgraded to a higher torque rating, by adding one of two options.

- 1. The MH6B.62D, or .75D offers a Single Caliper Dual Piston configuration, giving 1440 inch pounds of torque.**
- 2. The MH6BD.62, or .75 offers a Dual Caliper configuration, giving 2140 inch pounds of torque.**

Both the MH6B and the MH6B.75 utilize a tube type axle assembly for ease of installation. This axle can easily be placed in the tube assembly of the strut, pinned into place, and is ready to go. The axle is made of 4140 heat-treated steel to ensure maximum strength and durability. A flanged axle is available for the .75 wheels. The rims separate on the wheels to make mounting and dismounting an easy task. The wheels are available with either silver or gold anodizing.

PERFORMANCE

The MH Series wheels are designed for the following performance standards:

MH6B/6" & MH6B.75/6"

Static Capacity	660 pounds
Load Limit	2000 pounds
Max Accel/Stop (Kinetic Energy)	93,441 foot-pounds
Torque Rating @ 450psi	1070 inch pounds

MH6B.62D/6" & MH6B.75D/6"

Static Capacity	660 pounds
Load Limit	2000 pounds
Max Accel/Stop(Kinetic Energy)	93,441 foot pounds
Torque Rating @ 450 psi	1440 inch pounds

MH6BD.62/6" & MH6BD.75/6"

Static Capacity	660 pounds
Load Limit	2000 pounds
Max Accel/Stop(Kinetic Energy)	93,441 foot pounds
Torque Rating @ 450 psi	2140 inch pounds

MH6BDXT.75/6"

Static Capacity	660 pounds
Load Limit	2000 pounds
Max Accel/Stop(Kinetic Energy)	93,441 foot pounds
Torque Rating	3080 inch pounds

TIRE & TUBE

Any six-inch tire and tube combination can be used with this assembly. The more common combinations are the 15X600X6 2 ply or four ply tubeless for light use on paved surfaces. The 800X6 for soft and rough field landings, or the 600x6 aircraft tire for a higher profile and clearance.

B. MH SERIES WHEEL / PARTS LIST

BRAKE ASSEMBLY & BEARING CALLOUT

WHEEL	BRAKE ASSY	BEARINGS
MH6B	WHLB4-1	MSC1628DCTN
MH6B.62D	WHLB3-1	MSC1628DCTN
MH6BD.62	WHLB4-8	MSC1628DCTN
MH6B.75	WHLB4-2	MSC1630DCTN
MH6B.75	WHLB3-2	MSC1630DCTN
MH6BD.75	WHLB4-D.75MH	MSC1630DCTN
MH6BDXT.75	WHLB4-DXTMH	MSC1630DCTN

WHEEL PARTS LIST & NUMBERS (See Fig. 4)

NUMBER	PART NUMBER	DESCRIPTION	QNTY
18	MSC.31-18X1.25SHCS	Socket Hd Cap Screw	3
19	MSC10-24X.62SHCS(A)	Socket Hd Cap Screw D	3
20	MSC.31-18X.75SHCS	Socket Hd Cap Screw	3
21	MSCAN960-516L	Washer	12
22	WHLD4	Brake Disc 4"	1
23	MSC1628 or 1630 DCTN	Ball Bearings 62 / .75	2
24	MH62-1 or MH62-2	Hub w/.62 or .75 Brng	1
25	MH62-6-25B(A)	Wheel, Brake Half	1
26	MHML6	Mounting Lug	3
28	MH62-6-25H(A)	Wheel, Valve Half	1
29	MSC.31-18NYLOCK	Lock Nut	6
not on dwg	MSCLABELMATCO2	Label	1

C. BRAKE ASSEMBLY PARTS LIST

WHLB4-1 & WHLB4-2 (See Fig. 2)

NUMBER	PART NUMBER	DESCRIPTION	QNTY
1	MSC10-24X1.75SHCS(A)	Socket Head Cap Screw	2
2	MSCAN960-10L	Washer	4
3	MSC10-24X1.75SHCS	Socket Head Cap Screw	2
4	WHLB4-1	Stationary Brake Shoe	1
5	WHLB4-2	Stationary Brake Shoe	1
6	MSC4-6	Brass Rivet	2
7	WHLBSP4	Spacer 4" / UL	4
8	WHLBPA.75MH	Brake Plate .75 MH	1
9	MSC4-4	Brass Rivet	2
10	WHLB4-1	Movable Brake Shoe	1
11	WHLB4-2	Movable Brake Shoe	1
12	MSC2-218	O-ring Buna N	1
13	WHLPH-2	Puck Housing 4" / UL	1
14	MSC.234-X.50IL	Dust Plug	1
15	MSCF6446-007	Brake Bleeder Valve	1
16	MSCBBS(A)	Brake bleeder Seat	1
17	MSC10-24NYLOCK	Locking Nut	2
18	MSC2X	Cap Plug	1
19	MSCAN960-10	Washer	2

WHLB3-1 & WHLB3-2 (See Fig. 3)

NUMBER	PART NUMBER	DESCRIPTION	QNTY
1	MSC25-20X1.5SHC(A)	Socket Head Cap Screw	3
2	MSCAN960-416L	Washer	5
3	MSCAN4-17A	Bolt	2
4	WHLB3-1	Stationary Brake Shoe	1
5	WHLB3-2	Stationary Brake Shoe	1
6	WHLM66-102	Lining 4" / UL Dual	2
7	MSC4-6	Brass Rivet	2
8	WHLBSP40	Spacer 4" / UL .25 ID	4
9	WHLBPA.75MH	Brake Plate .75MH	1
10	MSC4-4	Brass Rivet	2
11	WHLB3-1	Movable Brake Shoe	1
12	WHLB3-2	Movable Brake Shoe	1
13	WHLPI-2D	Piston 4" / UL Dual	2
14	MSC2-210	O-ring Buna N 70 DUR	2
15	WHLPH-3	Puck Housing 4" / UL D	1
16	MSC.234-X.50IL	Dust Plug	1
17	MSCF6446-007	Brake Bleeder Valve	1
18	MSCBBS-16	Brake bleeder Seat	1
19	MSC.25-28NYLOCK	Locking Nut	2
20	MSC1X	Cap Plug 1/16	1

WHLB4-8 & WHLB4-D.75MH (See Fig. 4)

NUMBER	PART NUMBER	DESCRIPTION	QNTY
1	MSC10-24X1.75(A)	Socket Head Cap Screw	4
2	MSC10-24X1.75SHCS	Socket Head Cap Screw	4
3	WHLBSB4	Stationary Brake Shoe	2
4	WHLBSP4	Spacer 4" / UL Brake	8
5	WHLM66-103A	Lining 4" / UL Brake	4
6	WHLMBS4	Movable Brake Shoe	2
7	WHLPI-2	Piston 4" / UL	2
8	MSCBBS(A)	Brake Bleeder Seat	1
9	MSC.234-X.50IL	Dust Plug	1
10	MSCF6446-007	Brake Bleeder Valve	1
11	MSC4-4	Brass Rivet	4
12	WHLBPD.75MH	Brake Plate Dual .62	1
13	MSC2-218	O-ring Buna N	2
14	WHLPH-2	Puck Housing 4" /UL	2
15	MSC2X	Cap Plug	3
16	MSCAN960-10L	Washer	8
17	MSC10-24NYLOCK	Nylock Nut	4
18	MSC4-6	Brass Rivet	4
19	MSCAN960-10L	Washer	4

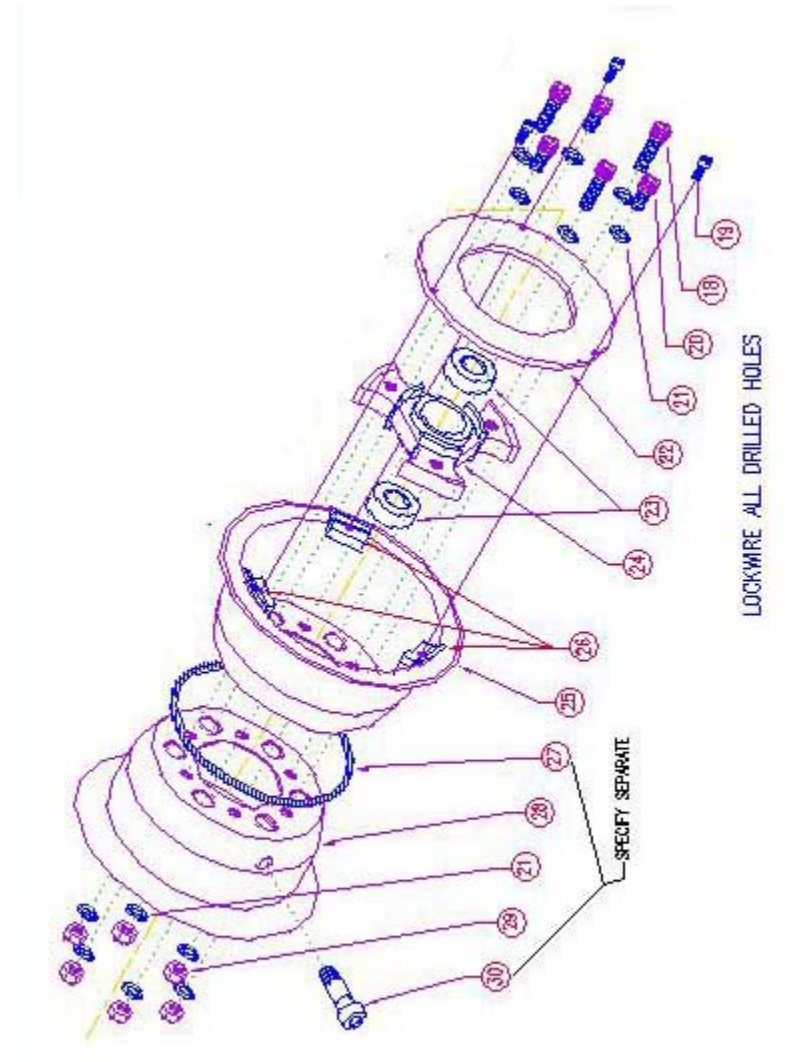
WHLB4-DXTMH (See Fig. 4)

NUMBER	PART NUMBER	DESCRIPTION	QNTY
1	MSC.25-20x1.75(A)	Socket Head Cap Screw	4
2	MSC10-24X1.75SHCS	Socket Head Cap Screw	4
3	WHLBSB4XT	Stationary Brake Shoe	2
4	WHLBSP4	Spacer 4" / UL Brake	4
5	WHLM66-103A	Lining 4" / UL Brake	4
6	WHLMBS4	Movable Brake Shoe	2
7	WHLPI-4	Piston 4" / UL	2
8	MSCBBS(A)	Brake Bleeder Seat	1
9	MSC.234-X.50IL	Dust Plug	1
10	MSCF6446-007	Brake Bleeder Valve	1
11	MSC4-4	Brass Rivet	4
12	WHLBPD.75MH	Brake Plate Dual .62	1
13	MSC2-218	O-ring Buna N	2
14	WHLPH-4XT	Puck Housing 4" /UL	2
15	MSC2X	Cap Plug	3
16	MSCAN960-10L	Washer	8
17	MSC10-24NYLOCK	Nylock Nut	4
18	MSC4-6	Brass Rivet	4
19	MSCAN960-10L	Washer	4
20	WHLBSP40S	Spacer 4" / UL Brake	4

D. WHEEL ASSEMBLY DRAWING

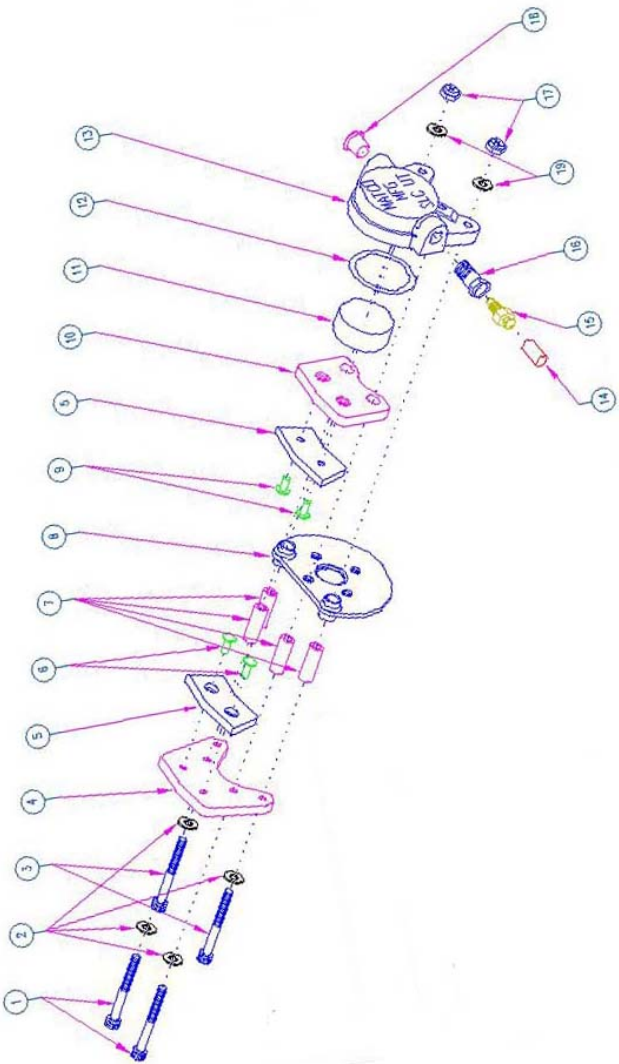
MH SERIES WHEEL ASSEMBLY

Fig. 1

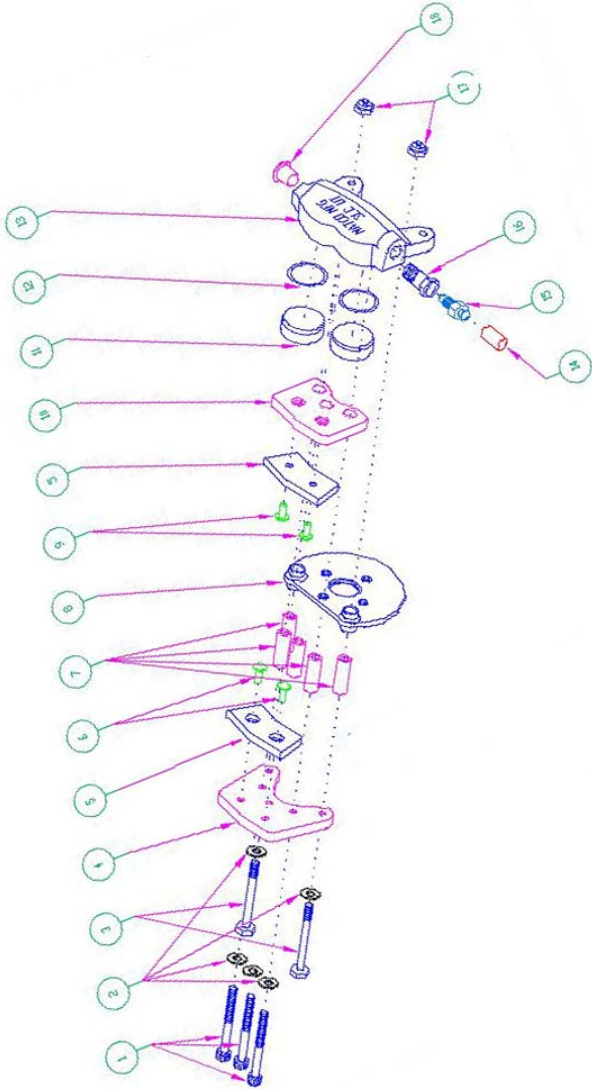


E. BRAKE ASSEMBLY DRAWINGS

**MH SERIES
SINGLE CALIPER, SINGLE PISTON
Fig. 2**

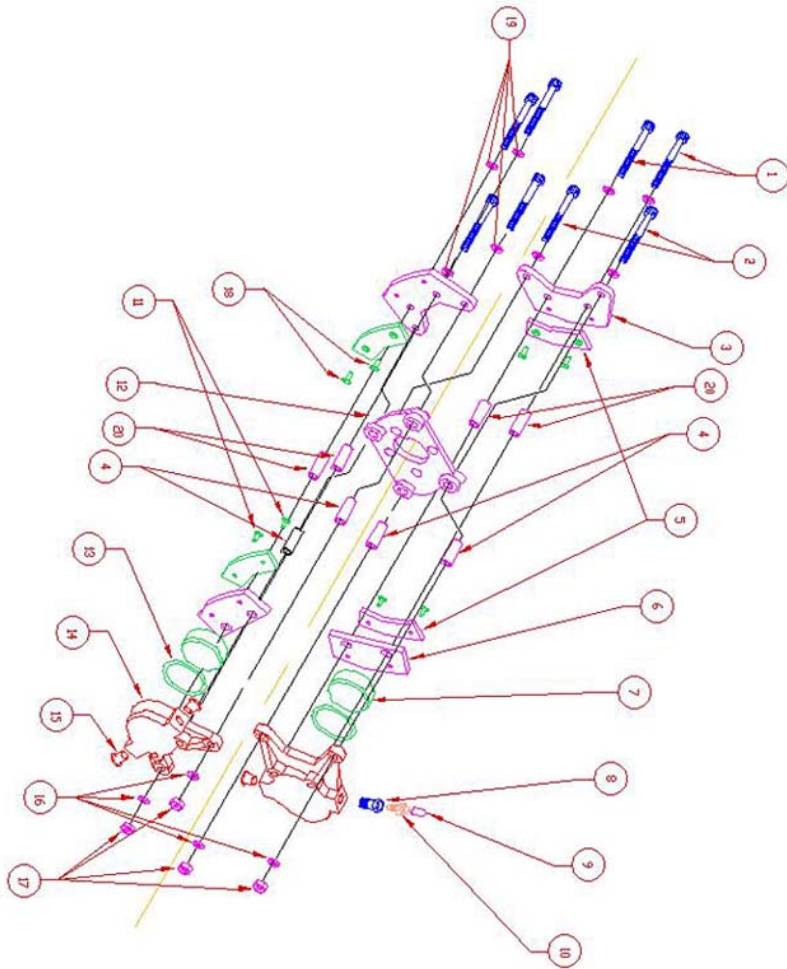


**MH SERIES
SINGLE CALIPER, DUAL PISTON
Fig. 3**



MH SERIES DUAL XT CALIPER ASSEMBLY

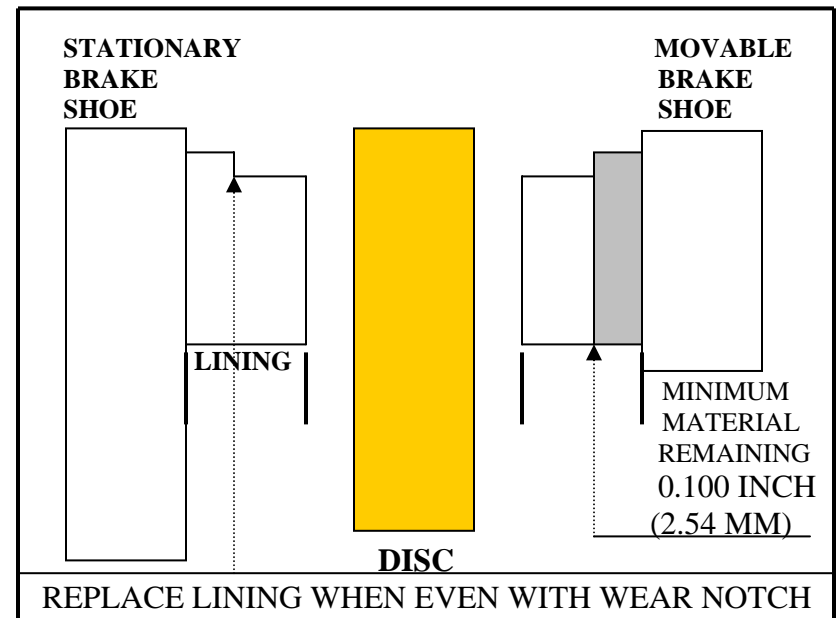
Fig. 4



F. BRAKE LINING WEAR LIMITS

To eliminate wear on brake linings beyond design limitation and reduce possible piston damage or fluid leakage, the following information is presented. The MH series lining should be replaced when the thickness of the remaining wear material reaches 0.100 IN. (2.54mm) See Fig. 5. The WHLM66-103A lining has a visible wear notch located on the end of the lining, and the WHLM66-1052 is located on the top. The inside edge of the notch indicates min-material condition.

Fig. 5



SwiftLine Pad Replacement Program for the WE51

The *Swiftline* Pad Replacement program is designed to:

- Simplify pad replacement on MATCO mfg brakes
- Eliminate the need to rivet linings, saving maint. & tooling.
- Provide a 20 % discount on reline kits saving you money

For more information on Swiftline call 801-335-0582

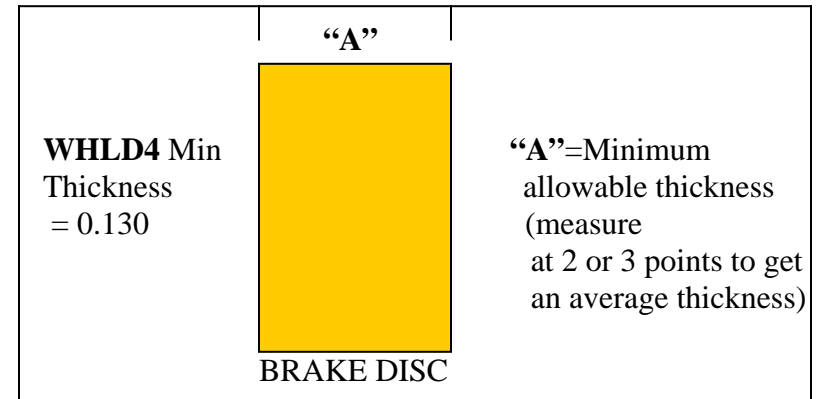
G. BRAKE DISC INSPECTION

The MATCO brake disc will give years of trouble free service under normal field conditions. Conditions such as unimproved fields, standing water, industrial pollution, or frequent use of the aircraft may require more frequent inspection of the brake system including the disc in order to prolong the life of the brake linings. The disc should be checked for wear (See **Fig. 6 Dim. "A"**) and for any grooves, deep scratches, excessive pitting or coning of the brake disc. Although coning is rarely a problem with the MATCO disc, if it should occur, coning beyond 0.015 inch (0.381mm) in either direction is cause for disc replacement. Isolated grooves up to .030 inch (0.76mm) deep should not be cause for replacement. Any grooving of the disk however, will reduce the service life of the linings.

The WHLD4 disc is plated for rust prevention. Within a few landings, the plating will wear off where the linings rub against the disc. The remaining portion of the disc will remain plated and corrosion free for an extended period of time under normal use. Chrome plated discs are available from MATCO for those demanding increased corrosion protection and wear.

Rust in varying degrees may form on the exposed portion of the disc. If powdered rust appears on the surface, one or two braking applications during taxi should wipe the disc clear. Build up beyond this point, may require removal of the disc from the wheel to properly clean both surfaces. Wire brushing followed by sanding with a 220-grit sandpaper should restore the braking surface adequately. Care should be taken to prevent removal of plating in areas that are not contacted by the lining.

Fig. 6



H. BRAKE LINING INSTALLATION

The following instructions offer a guide for properly removing and replacing the WHLM66-103A And the WHLM66-1052 brake linings.

1. Remove the caliper from the wheel by removing the two MSCAN4-17A bolts that hold it on.
2. Remove old linings by drilling the crimped side of the rivet (Do not use a punch & hammer). Using a #25 drill (0.1495 diameter), drill through rivet taking care to avoid damaging the rivet hole. After drilling crimped edge off rivets, lift old lining and remaining rivet pieces from the brake shoe.
3. Inspect the brake shoe for any bending or other damage that may have occurred during service. A shoe with more than 0.010 bend should be replaced. Inspect rivet holes to ensure that no damage has occurred during removal.
4. Using a brake relining tool (*MATCO recommends a Threaded Screw Action such as the W404 from Aircraft Tool SupplyCo.*) or pneumatic press, replace the lining using the brass rivets shown on the illustrated parts list.

I. MOUNTING THE TIRE & TUBE

Care should be taken when mounting the tire and the tube on the wheel so as not to pinch the tube between the wheel halves. Slightly inflate the tube after placing it in the tire. This will keep it from being pinched between the halves. Tire mounting soap may also help. A thin strip of cardboard or poster paper wrapped around the wheel between the mounting half and the tube will help in preventing the tube from being pinched during assembly if it is unusually tight. Another method is to use a strand of monofilament fishing line placed between the wheel and the tube, and running in the same direction as the axle. Move the line back and forth around the wheel as it is being tightened. When satisfied that the tube is clear of the wheel, simply pull it out.

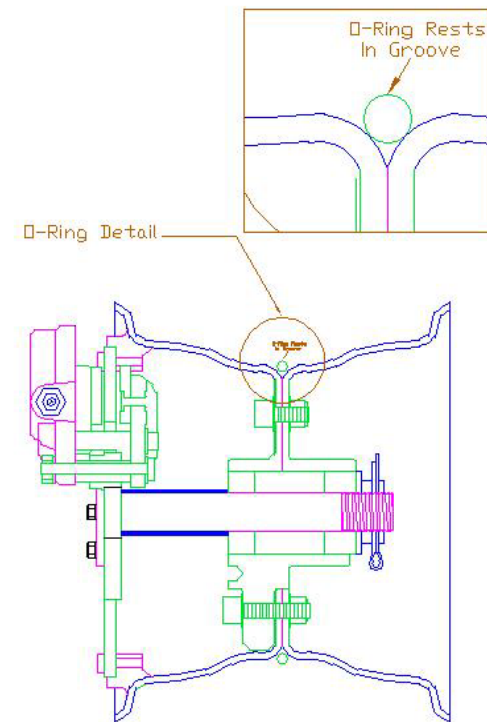
J. TUBELESS KIT INSTALLATION

1. Inspect the rim face at the radius where the o-ring will seat, for deep scratches, nicks or imperfections. Smooth out any imperfections with a medium grit emery cloth. **(Fig. 7)**
2. Insert valve stem into the 1/2" hole and pull through from the inside of the rim. A rubber lubricant or soap and water solution may make it easier to install.
3. Take the brake half rim (*the one without the valve stem hole*) and insert it through the tire opening that will face towards the landing gear. Push the large o-ring over the diameter of the rim inside the tire and roll it back approximately 1 inch from the mating surface of the rim. Insert the other rim (*with the valve stem*) in what will be the outside of the tire assembly. Bolt the rims together with the

three 5/16-18x.875 socket head cap screws, washers and nuts supplied spaced in every other hole.

4. Roll the o-ring to the center of the rim assembly. This is done by pushing the tire bead down evenly on the brake half side until it reaches the mating point of the two rim halves. The o-ring will seal the joint against leaks.
5. Coat the bead mounting areas of the tire and rim with suitable lubricant and inflate the tire to specification.
6. Install the remaining 5/16-18 nuts and washers on hub bolts and install the hub.

Fig. 7



K. MH WHEEL ASSEMBLY

ASSEMBLY INSTRUCTIONS FOR MH SERIES WHEEL:

1. The axle nut should be tightened until all play is out of the assembly. Rotate the wheel back and forth while tightening the nut to until the nut is tight against the bearings. When all play is out of the assembly back off to the next castle slot and insert the cotter pin. The wheel should spin freely.
 2. All o-rings in the brake and master cylinder, are Buna Nitrile and are **NOT** compatible with automotive glycol based brake fluids such as DOT 3, DOT 4, and DOT 5.1
- NOTE** USE ONLY red aircraft fluid (Mil-H-5606) brake Fluid or its equivalent.
3. The ideal mounting position for the brake caliper is the trailing side of the wheel with inlet and bleeder in a vertical axis. However, the caliper may be mounted at any location as long as the system can be bled of air properly.
 4. When using MATCO mfg. flanged axles, they can be shimmed for toe-in or toe-out conditions, and spaced out from the wheel if necessary for the brake disk attachment screws to clear the landing gear leg. MATCO mfg. axle material is heat treated steel and cannot be welded.

L. ASSEMBLY TORQUE VALUES

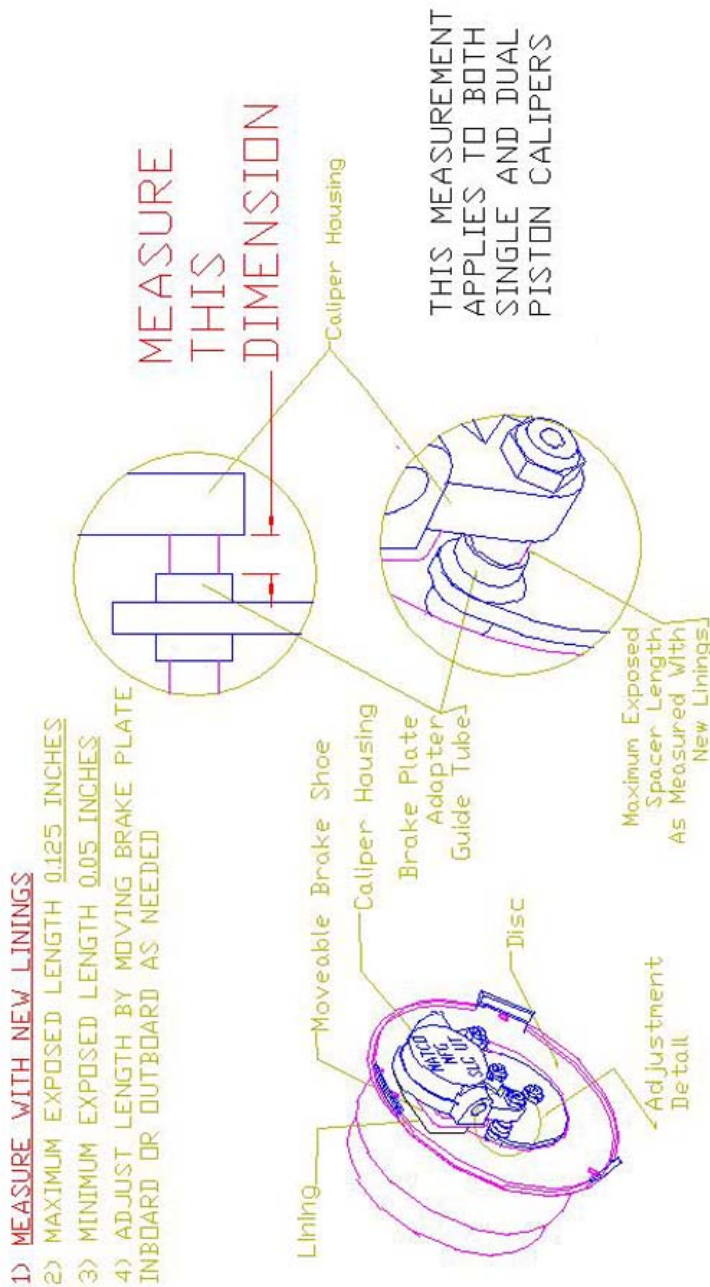
Fig. #	Item #	PART NUMBER	TORQUE VALUE (INCH LBS.)
2	1	MSC.10-24X1.75SHCSA	60 INCH Lbs
2	17	MSC10-24NYLOCK	100 INCH Lbs
3	1	MSC.25-20X1.5SHCSA	80 INCH Lbs
3	17	MSC.25-28NYLOCK	100 INCH Lbs
1	19	MSC10-24X.62SSHCS	100 INCH Lbs
1	29	MSC.31-18NYLOCK	160 INCH Lbs
1	18	MSC.31-18X1.25SHCS	80 INCH Lbs

M. CALIPER ALIGNMENT

Caliper alignment is determined by measuring the maximum exposed spacer length, as measured on a new set of linings. (See **Fig. 8**)

1. Maximum exposed length should be 0.125 inches.
2. Minimum exposed length should be 0.05 inches
3. Adjust the length by moving the plate inboard or outboard as needed to reach proper measurement.
4. Note that this measurement applies to both single and dual piston calipers.

Fig. 8



N. BLEEDING THE BRAKE SYSTEM

1. Open brake bleeder valve slightly (**Fig. 2 & 3 # 15. Fig. 4 # 10.**) to facilitate bleeding of air from the system.
2. Attach a tube from the nozzle of a squirt can (such as the MATCO squirt can part # MSCCHPSS) of brake fluid, to the top of the brake bleeder valve. Pump the handle until oil flows bubble free from service hose before attaching.
3. Make sure that the master cylinder shaft is fully extended to open up the internal bypass valve.
4. Inject brake fluid (Mil-H-5606) or equivalent, into the puck housing and continue injecting until the fluid travels through the system in to the master cylinder.
5. Air in the system will be pushed up and out in to the master cylinder ONLY IF the master cylinder or remote reservoir is at the highest point in the system, and there are no loops in the brake lines.
6. Fluid should be pushed through the system until it reaches approximately $\frac{1}{4}$ inch from the top of the master cylinder or remote reservoir
7. Close the brake bleeder valve, and remove the service hose.
8. If the brake system is free of air, the brake pedal should feel firm and not spongy. If not, repeat steps 1 through 7 until system is free of trapped air.
9. Fluid leakage from the top of the MCMC-5 / 5A master cylinder during operation indicates too high a fluid level.

NOTE The MCMC-5/5A are NOT approved for inverted flight.

O. CONDITIONING PROCEDURES

NOTE It is important to condition the new linings after installation to obtain maximum service life and performance. The procedures below show when and how this should be done.

1. After the linings have been installed, apply brake pressure during high throttle static run-up. Note RPM at creep if any occurs.
2. Perform two or three taxi stops from approximately 30-35 mph to generate 300 – 400 degrees at brake pads. Allow brakes to cool for 10-15 minutes.
3. Repeat step one and note RPM at creep if any occurs. There should be a noticeable increase in holding torque.
4. If properly conditioned, the pads will have a uniform shiny appearance (*glaze*) on the surface.

NOTE forward movement of the aircraft while testing brakes, could be caused by skidding and not brake malfunction. Use caution when breaking heavy on aircraft with a tail-wheel as it could cause the tail to lift from the ground.

Conditioning removes high spots, and creates a layer of glazed material at the lining surface. Normal braking will produce enough heat to maintain glazing during the life of the lining. Glazing can be worn off during light use such as taxiing.

P. MAXIMIZING BRAKE OUTPUT

GETTING YOUR PEDAL GEOMETRY RIGHT

BRAKE SPECIFICATIONS

All MATCO mfg. brakes have two specified ratings. The first is the energy rating which specifies the energy capacity of the brake. This value is used in selecting a brake that will be able to absorb the kinetic energy of the aircraft under the designers specified maximum energy condition (*generally maximum aircraft weight at a velocity above stall speed*). The energy rating is determined by the disc weight. Exceeding the energy capacity of a braking system leads to excessive disc temperatures. This can cause low friction coefficients and reduce brake torque and aircraft deceleration. Permanent damage to the disc can result in the form of warping or loss of corrosion protection.

BRAKE TORQUE

The second rating is for brake torque. The rated torque value is used to determine the deceleration and static torque for engine run-up that will be provided by the brake. A braking system using the same disc can have one energy rating and several torque ratings. This is possible by using different caliper configurations on the same disc. For example a braking system using a single caliper on a disc with a 189K ft-lb rating may have a torque rating of 1980 in-lb. The same braking system using two calipers would have the same energy rating of 189K ft-lb but would have a torque rating of 3960 in-lb. MATCO mfg. offers its customers a wide range of caliper configurations and disc sizes to allow for meeting both the energy and torque requirements of their aircraft. (*Look under Features on page 3 for more information on caliper options*).

GETTING THE RATED TORQUE

The rated torque value assumes a nominally conditioned brake pad (*see pad conditioning procedures section 'N'*), rated pressure applied to the brake, free floating calipers, and pad contact on both sides of the disc. Brake pad conditioning allows a glaze to form on the pads and provides the highest friction coefficient and drag force. MATCO mfg. Brake torque ratings are based on 450 psi applied pressure. Pressures below this value will generate proportionally lower torque. Pressures above this value will provide higher torque although pressures above 600 psi generally cause caliper deflections that reduce the torque increase. The torque rating assumes that all caliper force is used to squeeze the brake pads against the disc. If the caliper does not float freely, it is possible that only one side of the disc surface may be contacted resulting in 50% loss of torque.

GET THE PRESSURE RIGHT

Assuming the calipers are properly mounted so that the pads make contact on both sides of the disc (both new and worn) and are maintained so that the calipers float freely, the most common reason for under performance of the brakes is low pressure. MATCO mfg. Brakes need 450 psi to achieve their rated torque. Additional calipers can be added to get higher torque at lower pressures, but is often more weight efficient to modify the hydraulic system pedal geometry to generate higher pressures. Systems using hand or foot operated master cylinders require a minimum of 2.5 to 1 mechanical advantage when using master cylinder, MC, like the MC-4 or MC-5 which have .625 inch diameter pistons. (*Systems using MC-4 or MC-5 with intensifiers have .500-inch pistons and require a 1.6 to 1 mechanical advantage*). Mechanical advantage, MA, is the ratio of the force applied to the master cylinder shaft divided by the force applied by the hand or foot. **Dia.1** shows two examples of pedal geometry. The first has an MA of 1 to 1 since the distance from the applied load to the pivot point is the same as the distance to the MC and is undesirable.

The second shows a more favorable configuration that will easily provide the required pressure to the brakes with moderate toe force.

It is often necessary to keep the foot pedal shorter than that shown in **Dia.1**. An alternate geometry is shown in **Dia.2**. This design would utilize a fork arrangement on the MC connection to allow clearance of the MC body and then a short linkage to the MC connect point. A design common to many aircraft uses linkage as shown in **Dia.3**. This design also allows for a shorter brake pedal but has a major disadvantage. This linkage can be configured to have a proper MA in the start position (with the master cylinder fully extended). The MA varies with rotation however, as shown in **Fig.2** of **Dia.3**, a 15 degree rotation of the linkage reduces the MA at the start position from 1.5 to 1 down to only 1.12 to 1. In actual operation, this has the effect of causing a nearly constant brake torque even though increasing force is applied. For example, if the geometry is set for an initial MA 2.5 to 1. In the start position and the pilot applies pedal force, the MC will begin to stroke as pressure builds. As the rotation occurs, the MA decreases. If there is any air in the brake lines or if there are long brake line runs, hydraulic system expansion will occur as pressure increases requiring more MC stroke. If the pilot applies more pedal force, more MC stroke occurs, and the MA decreases further. Even though the pilot has now increased his pedal force, the force applied to the MC will be only marginally increased because more rotation will result and cause a further decrease in MA. A geometry like that in **Dia.2** will provide the same reduced pedal height and is not prone to the effect of rotation since the MC is essentially connected to the brake pedal pivot. **Dia.4** illustrates the benefit of pivot connect geometry during rotation. The MA remains virtually unchanged for expected rotation angles and results in a linear pressure increase with applied pedal force.

HEEL BRAKES

A common means of providing pilots with differential braking ability without resorting to a more complicated geometry of toe brakes is to use heel brakes. The same design requirements exist for the MA of a system using heel brakes as for toe brakes. It is not uncommon to see MC's configured to allow the pilot to apply heel force directly to the MC by means of a pad or button connected on the end of the shaft. This configuration is shown in **Fig.1** of **Dia.5**. The MA of this system is 1 to 1 and produces very low pressure for reasonable heel force. Perhaps a larger concern however is the potential for causing damage to the MC. The MC is designed to accept loads applied along the length of the shaft. Loads applied off axis or perpendicular to the shaft cause bending moments in the MC shaft that it is not designed for. Damage to the MC end gland, or bending of the MC shaft may result if the off axis loads are high enough. A more desirable configuration for heel brakes is shown in **Fig.2** of **Dia.5**. This system uses a short linkage connected to the MC that provides the 2.5 to 1 MA while insuring that loads will be applied along the length on the MC and prevent any damage during actuation.

CONCLUSION

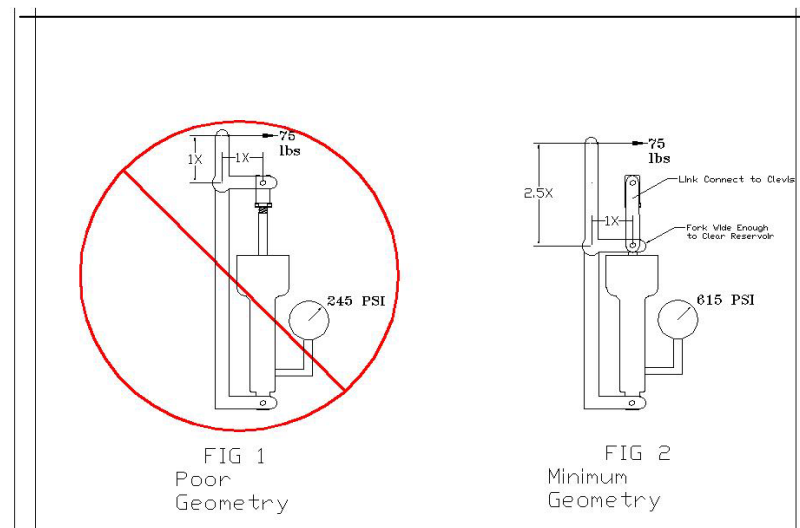
Like any system on an aircraft, the hydraulic system has many engineering options for providing the necessary requirements. The systems common on light aircraft must be engineered to provide adequate pressure to the brakes to achieve the rated torque.

NOTE MATCO mfg. Brakes require 450 psi to achieve Their rated torque.

The pedal geometry whether hand, toe, or heel operated, requires a mechanical advantage of at least 2.5 to 1. This allows the pilot to easily generate the required 450-psi with moderate applied force. Pivot connected geometry provides the best means of accomplishing this requirement without the problem of rotational effect that reduces mechanical advantage.

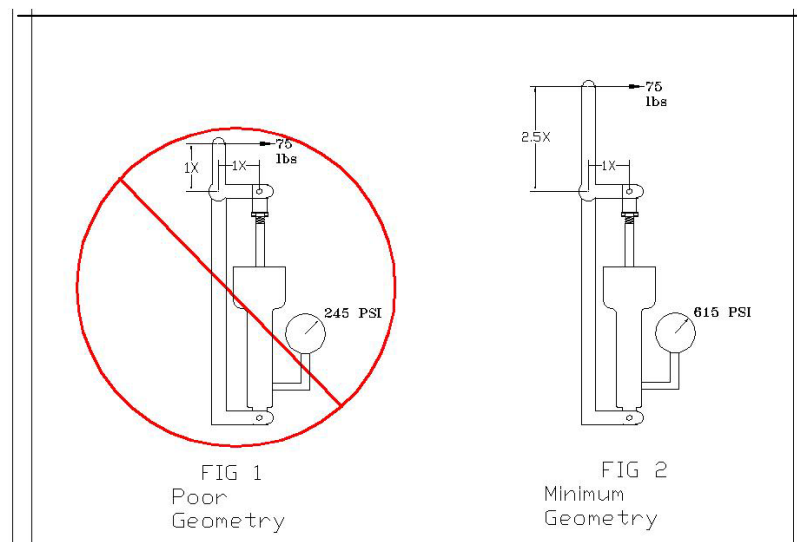
PEDAL GEOMETRY / POOR & MINIMUM

Dia. 1 Figures 1 & 2

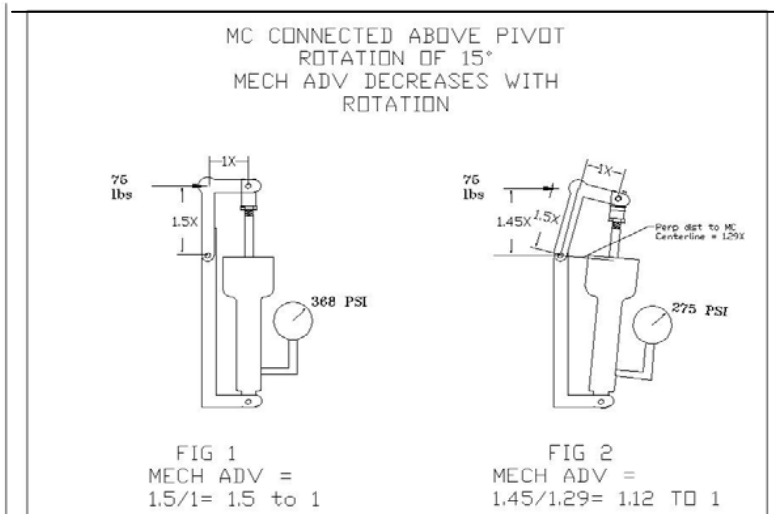


PEDAL GEOMETRY / POOR & MINIMUM

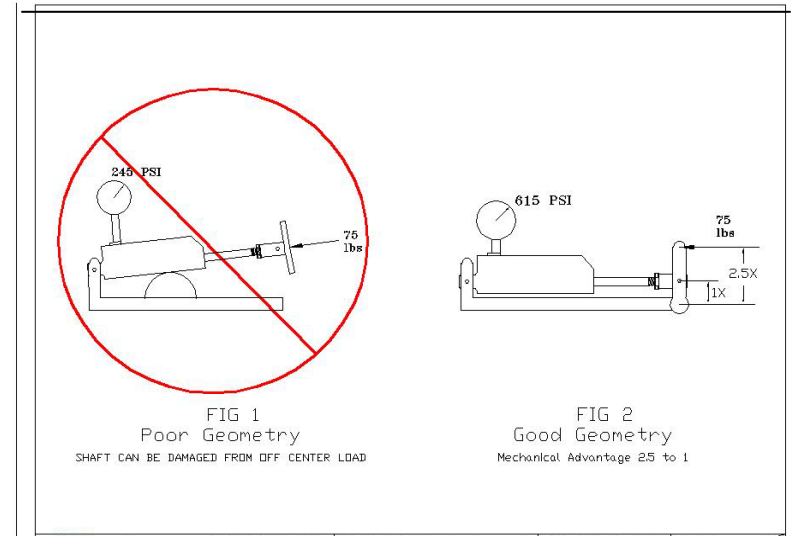
Dia. 2 Figures 1 & 2



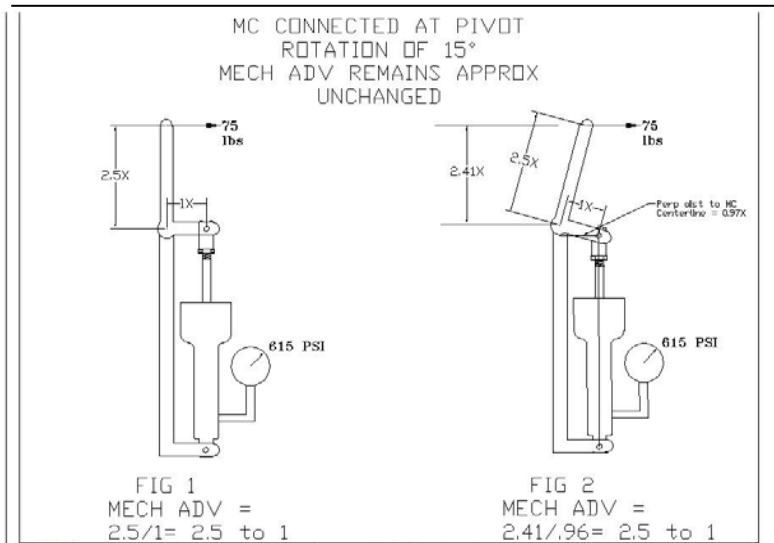
PEDAL GEOMETRY / MECHANICAL ADVANTAGE
Dia. 3 Figures 1 & 2



PEDAL GEOMETRY / HEEL BRAKES
Dia. 5 Figures 1 & 2



PEDAL GEOMETRY / PIVOT CONNECT
Dia. 4 Figures 1 & 2



Q. LUBRICANTS

ELASTOMERIC COMPOUND LUBRICANTS

HYDRAULICS: MIL-H-5606 / MIL-H-83282
Or equivalent (Red Oils)

NOTE DOT 5.1 brake fluid is NOT compatible with MATCO mfg brakes, and will damage the Buna-N o-rings used in the system.

PETROLEUM LUBRICANTS

WHEEL BEARINGS: MIL-G-81322
MOBIL 28
AEROSHELL 22
Or equivalent lubricants

AMPHIBIOUS: HCF Grease P/N 605
BG Products, Wichita, KS.

WHEEL NUTS / BOLTS: MIL-T-5544 Antiseize
Or equivalent

THREAD SEALANT

TAPERED PIPE THREADS: Loctite 567, or
equivalent

R. TECHNICAL ASSISTANCE

For technical Information, Product Matching, and Helpful Hints, see our website at:

www.matcomfg.com

E-mail our technical service manager
for specific information at:

tech@matcomfg.com

TECHNICAL ASSISTANCE

To speak with someone in person about specific products or to find answers to technical questions, please contact us at our

TECHNICAL HOTLINE

801-335-0582

OR FAX US AT 801-335-0581

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